



## Applicability of composite and nanocomposite materials to reusable liquid propellant tanks

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## **OUTLINE**

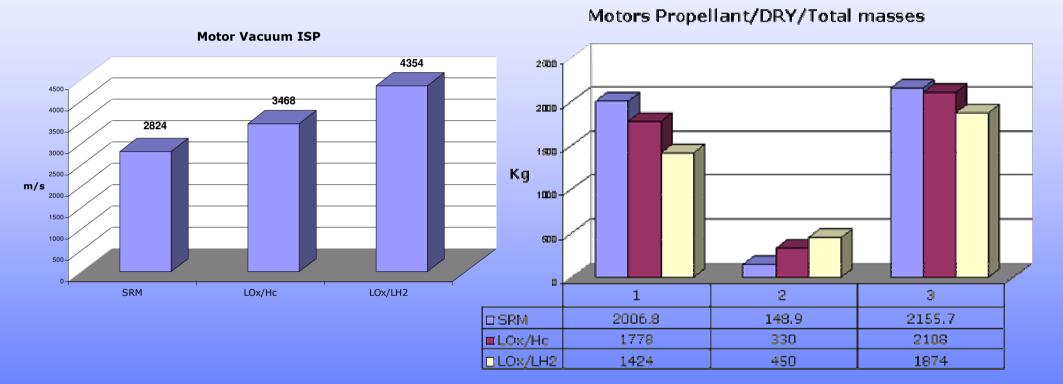


- Frame and Introduction
- CIRA previous experience
- Status of the Project
- Future work





Liquid propulsion based on LH2/LOX or LHC/LOX is expected to be the standard for next generation of reusable launchers



Looking at mass distribution it is evident that a reduction in tank weight could be the key improvement to RLV cost reduction



Prague September, 8 -5 2005, EUROMAT

Metallic cryotanks, based on Al-alloys, represent the mature technology for cryogenic propulsion.

Lightweight composite materials can potentially assure significant mass and cost reduction: they took advantage of an high specific strength and the possibility to be employed in automated manufacturing processes (i.e. Filament winding) far less expensive than conventional techniques used with metal alloys.







## <u>CIRA promoted "Cryo" project in the frame of</u> <u>USV PROGRAM</u>

The project has the final objective of designing, manufacturing and testing of a scaled demonstrator composite tank for LOX aimed at:

- Weight reduction (Composite Structure)
- Manufacturing cost reduction (Filament Winding)



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## **Technology Needs**

To contain, without leakage, cryogenic propellants for times required by launch mission.

Very low temperature (90 K) and high cyclic thermal loads ( $\Delta T_{max}$ = 300 K)

To sustain a suitable number of flight/abort cycles. Reusability RLV requirement and Air-frame integration

Carrying capacity of structural loads as well as internal pressure, axial and lateral inertia loads, which the launcher is subject to during the acceleration phase

Suitable permeability in order to border the liquid leakage rates within the limit set for the specific safety requirements

Feasibility property in relation to the fabrication limits imposed by the technological processes employed in modern manufacturing industries.

#### **INTRODUCTION - OBJECTIVE**



#### **TANK REQUIREMENTS**

#### DIMENSIONS

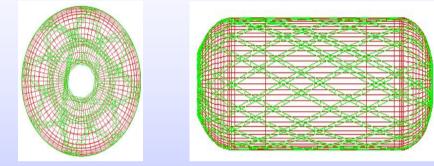
Cylindrical Height

Cylindrical Internal Diameter 540

Thickness (reference value)

8000 mm 5400 mm

3.5 mm



#### **TANK DESIGN HYPOTHESIS**

#### 1 - Linerless tank

All loads, chemical resistance and barrier performances are demanded to CFRP.

#### 2 - "Linered" tank

Load resistance is demanded to CFRP. Chemical resistance and barrier performances are demanded to the internal liner.



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•CFRP BESFIGHT IM600/Q133

•Plaster mandrel





#### •<u>Design</u>

Design optimisationCure cycle optimisation





#### Tank design

An aided design of the tank was realized using a filament winding simulation code (ARIANNA).



#### Ground testing Reusability critical areas

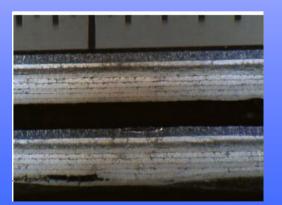


Temperature behaviour



Permeability

#### **Micro cracking**



Voids at leakage points

During the test campaign some leakage points were detected :

Pre-preg ageing
Not well adjacency among fibres.

Process quality control and <u>understanding of</u> basic phenomena!!

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Applicability of nanocomposite materials as internal liner.



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➤ The laboratory scale tests are carried out with the double aim to provide a database, as complete as possible, in order to support the FE design phase of the tank, and to identify the influences that typical CFRP parameters, such as Tg, kinetic cure, CTE, mechanical properties, density cracks etc. have on the cryogenic behaviour of the material as well as on its barrier performances.



The laboratory testing involves:thermal analysis,optical and electron microscopy,

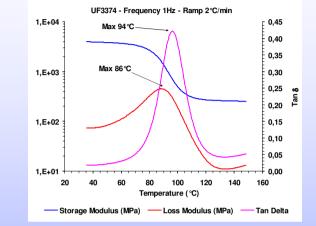
- •mechanical testing,
- barrier property characterisation.





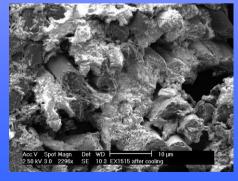
## Characterization laboratory-scale: Thermal analysis

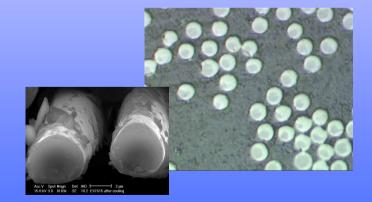
This work has addressed the issue of understanding the processing limit of B-staged tow prepreg candidate for cryogenic application and defining their optimal cure cycles.



#### Characterization laboratory-scale: non destructive analysis

NDE, optical and electron analysis have been performed in order to optimize the process manufacturing and to evaluate cracks and defects in the sample specimens prior and after cryogenic exposure.





Cooling effects: local fiber/matrix debonding



## Mechanical tests

Test matrix

E,	LONGITUDINAL YOUNG'S MODULUS	
$\sigma_1^{R}$	LONGITUDINAL TENSILE AND COMPRESSION STRENGTH	
E <sub>2</sub>	TRANSVERSE YOUNG'S MODULUS	
$\sigma_2^{R}$	TRANSVERSE TENSILE AND COMPRESSION STRENGTH	
σ <sup>a</sup>	APPARENT TENSILE STRENGTH	
<b>G</b> <sub>12</sub>	IN-PLANE SHEAR MODULUS	
τ <sub>12</sub>	IN-PLANE SHEAR STRENGTH	





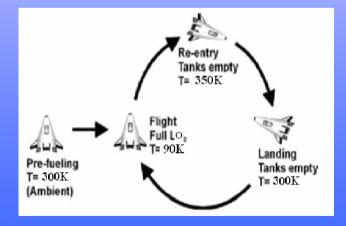
#### PRISTINE

#### CONDITIONING A

6-hours immersion in liquid nitrogen

#### CONDITIONING B (10 times)

Quenching from 300K to 77K by immersion in liquid nitrogen for 6 hours Heating up to 300K Heating up to 350K in 10 minutes Cooling back to 300K

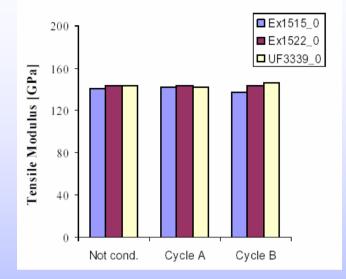




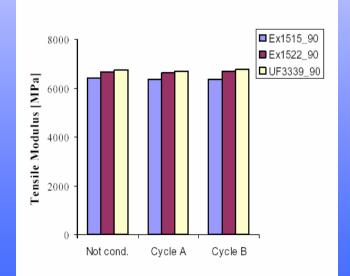
As thermal cycling is introduced to the laminate, one would expect for the value of Young's modulus to decrease if cracks were forming, since the bounds holding the material together are breaking apart effectively making it less stiff.

After reviewing all of the data, the conclusion was that the selected advanced materials, does not exhibit any crack growth after 10 cycles of the launcher flight.

Mechanical tests on the selected CFRP materials will be performed at 90K using a cryogenic mechanical testing machine (Colonnetti CNR Turin).



Longitudinal tensile tests





> The mass transport behaviour represents the main concern when thinking of polymer composites as materials for tank building. A barrier performance even a bit less than optimal could actually lead to a dramatic failure of the tank.

> Moreover, the polymeric matrix is characterised by a non-zero permeability to low molecular weight gases, which has to be measured and be kept under allowable values.

➤ The barrier performance can be estimated at different levels ranging from the macroscopic behaviour to the intrinsic material-related phenomena (multi-scale approach):

✓ leakage phenomena

✓ permeability behaviour

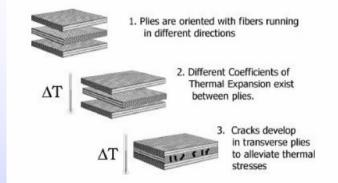


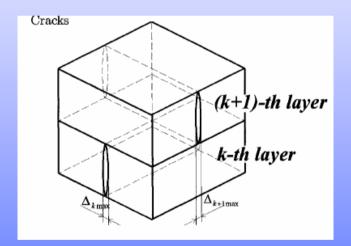
## Mass transport behaviour characterisation

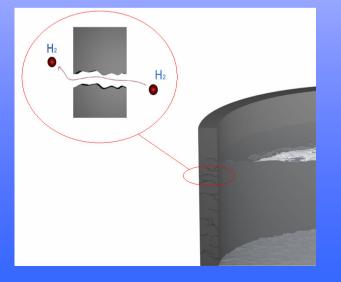


➤ The extension of composite materials to cryogenic tank building is not an ordinary issue. Composite materials particularly suffer from severe thermal stresses, which may cause matrix micro-cracking.

> In the case of leakage, gas or liquid flows through the leak path consists of continuously connected matrix cracks in each layer, which results in a sequence of connecting passages between both sides of the laminate.





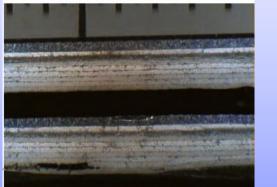


➢ Increase of the propellant leakage can be cause by the enlargement of crack-opening displacements caused by mechanical and thermal loads, increase of crack density and decrease of temperature.

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#### Leakage phenomenon

 $\succ$  The leakage test is necessary as it recreates the operative conditions of the actual tank, and serve as an evaluation tool for the effectiveness of both material and process parameters.





➢ In the leakage phenomenon the effects of intrinsic permeability, defects formed during the manufacturing process and microcracking arising from thermal cycling load are merged.



Water proof test up to 6 bar on a UF3339/IM7 tank-like specimen with  $\pm$  50 lamination sequence, previously conditioned. No cracks or leakage areas were observed.

## Diffusion/permeability

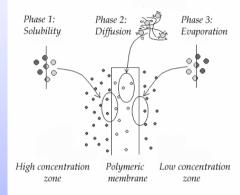
 $\succ$  If there are layers without cracks in the laminate, leakage does not take place, and diffusion alone can be present.

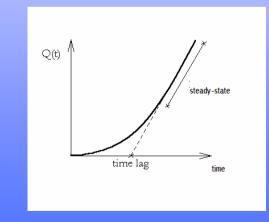
> The permeation through a polymer is a thermodynamic process. It involves:

the solubilitythe diffusionthe dissolution

The Time Lag Method allows one to determine the permeability (P), solubility (S), and diffusivity (D) coefficients. The time lag is simply the amount of time required for a gas to permeate through a membrane.

The integral technique measures the accumulation of the permeate gas (pressure) as a function of time.

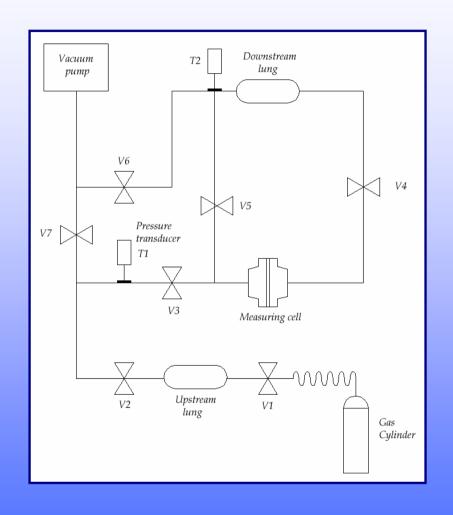




> The data is separated into two sections, the first region representing transient diffusion and the second steady-state diffusion.

## Mass transport behaviour characterisation







Preliminary permeability experiments have been performed: solubility, diffusion and permeability in the membranes have been evaluated in the 30°-80°C temperature range. The data at cryogenic temperature can be estimate by the Arrhenius-type relation.

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# Nanocomposite, in cryogenic propellant storage, could provide:

increased stability by preventing chemical degradation in aggressive liquid fuel environments

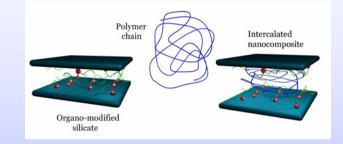
➢ increased gas barrier properties, originated by an increase in the diffusive path that a penetrant molecule must travel in the presence of filler and a decrease in mobility of macromolecules driven by interaction between nanoparticles and polymeric chain.

better mechanical properties



#### Type of nanocomposites considered in this work

Polymer-layered nanocomposites are produced promoting the intercalation of the polymer chain, or of a subsequently polymerized precursor, within the galleries of layered host crystals, organo-modified in order to enhance their affinity with the polymer.



#### RESINS

- EC97 produced by Camattini, Italy, (polyurethane epoxy-terminated resin having a reduced gas permeability)
- > DER 331 produced by DOW, that is an epoxy resin

#### NANOFILLER

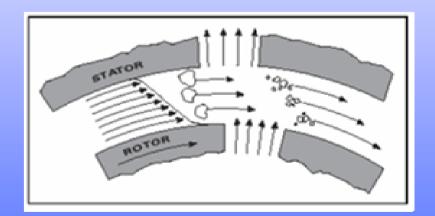
- > Hydrotalcite PURAL MG61HT from SASOL (moral ratio Mg/Al = 2/1) modified in house with ABS.
- > Dellite AP (commercial organo-modified montmorillonite produced by Laviosa Chimica, modified with a primary ammonium salt)

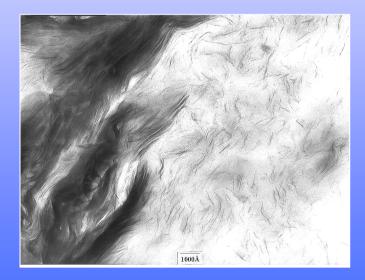


## **Nanocomposite Sample Preparation**

The polymer-clay mixtures were dispersed with a high performance dispersion device (Ultra turrax D25 basic, IKA WERKE) with a S25N-18G dispersion tool for 5 to 10 minutes at a variable speed ranging from 13500 to 24000 rpm.

Mechanical blends at 3 and 6wt% of each nanofiller were prepared for each of the two matrices selected





**Platelets Peel Apart** 



## Nanocomposite Sample Characterization Permeability

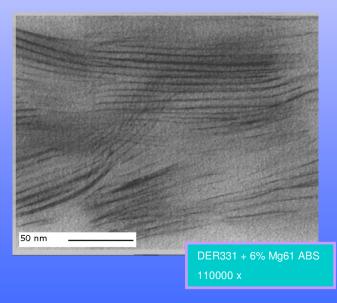
System	Average Permeability (cm <sup>3</sup> xcm/cm <sup>2</sup> xsecxPa)
DER 331	2,72E-15
DER 331+ 3% Mg61ABS	2,61E-15
DER 331 + 6% Mg61ABS	2,22E-15
DER 331+ 3% Del AP	2,58E-15
DER 331 + 6% Del AP	2,50E-15

EC97	8.19E-15
EC97 + 3% Mg61ABS	7,51E-15
EC97 + 6% Mg61ABS	5,47E-15

Measure performed with a MOCOM OX-TRAN 2/60 (carrier flux: 10cc/min; sample surface area: 10 cm2; T=23°C)

$$\frac{P_n}{P_p} = \frac{1 - \phi_s}{1 + \frac{2L}{6W}\phi_s \left(S + \frac{1}{2}\right)}$$

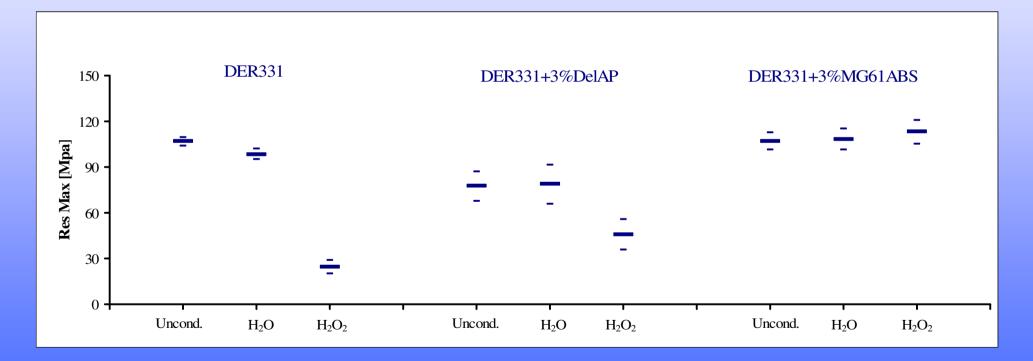
Bharadwaj model (2001): *Pn/Pp* is the relative permeability, *L* and *W* are the mean diameter and the thickness of the platelets,  $\phi_s$  is the volumetric fraction of platelets, *S* is an order parameter





## Nanocomposite Sample Characterization Chemical resistance

> Preliminary tests at ambient temperature were performed by evaluating nanocomposites mechanical properties (flexural) prior and after exposure to hydrogen peroxyde.



The addition of 3wt% of nanoclay prevent from matrix degradation



> The selected composite materials does not show matrix microcrack, delamination or increase of the porosity size caused by the thermal cycles at cryogenic temperatures. This aspect is very important to prevent leakage phenomena in the tank wall and to satisfy the reusable requirements.

The preliminary results obtained on nanocomposite materials show significant improvements in:

 $\checkmark$  the barrier properties

 $\checkmark$  the chemical resistance to oxygen

> An on-ground qualification campaign will be performed with liquid oxygen on the final scaled prototypes with the aim to verify the compliance of the project product with the fixed requirements.



## Thank you for your attention!