



Modelling oriented experiments: Behaviour of Fe-Cr-C model alloys under neutron irradiation

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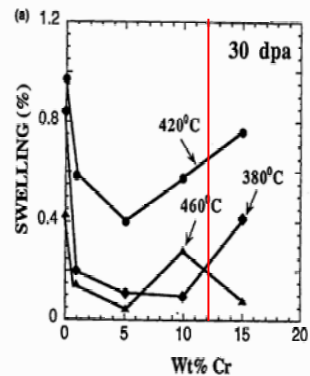
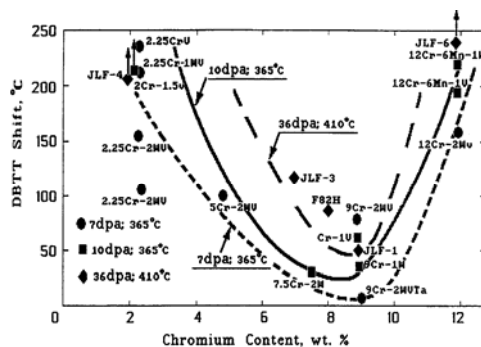
Introduction

In Fusion technologies:

Operating conditions	Properties needed
<p>Temperature (200 to 550°C)</p> <p>High flux and high dose (100 to 200 dpa); high He/dpa production rate (3 to 15 appm/dpa)</p> <p>High stress level (100 MPa)</p>	<p>High thermal conductivity and heat resistance; low thermal expansion</p> <p>Low DBTT shift; sufficient strength with limited loss of ductility and toughness; low swelling rate</p> <p>High creep resistance</p>



Why 9% Cr ?



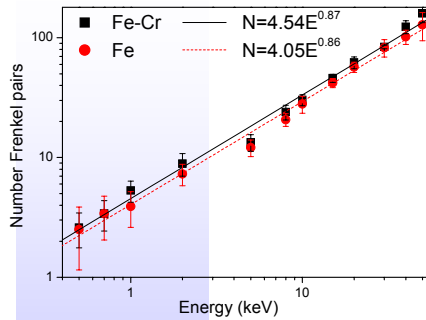
Lowest DBTT shift was found for 9% Cr steels → material is less brittle

Low swelling for Cr-content between 5 and 10%

Fe-9%Cr seems to be the best candidate

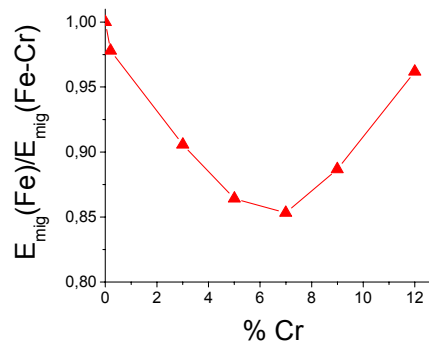
Effect of Cr on defect production and migration

Molecular Dynamic Simulation by D. Terentyev et al.



However: the presence of Cr affects strongly the diffusivities of irradiation induced defects

Cr has almost no effect on defect production rate



Objectives

- To assess experimentally the effect of Cr – concentration on defect production and accumulation in model alloys: how do they compare with steels under irradiation?
- To investigate the mechanisms of irradiation induced changes of the mechanical properties of high Cr F/M steels
- **Ultimate aim:** Provide reliable experimental database for model validation



Approach

- Experimental investigation of Fe, model alloys of different Cr content and industrial steels after neutron irradiation (same neutron flux, doses & temperature):

We chose as matrix:

- I- Pure Fe and ultra-pure Fe-9Cr
- II- Industrial pure Fe and Fe-2,5,9,12 Cr
- III- Conventional and LA Ferritic martensitic steels



Investigated Materials with chemical composition and heat treatment

Alloy	Mn	Si	P	Si	Al	Ti	Cr	Ni	Cu	Nb	B	Mo	C	N	V	W
251	0.009	0.02	0.013	0.0020	0.003	0.004	2.5	0.044	0.005	/	/	/	0.008	0.0173	0.001	/
259	0.02	0.04	0.011	0.006	0.0033	0.0028	5.04	0.06	0.01	/	/	/	0.02	0.0344	0.001	/
252	0.03	0.09	0.012	0.00066	0.0069	0.0034	9	0.07	0.01	/	/	/	0.02	0.0353	0.002	/
253	0.03	0.11	0.05	0.006	0.003	0.0037	11	0.09	0.01	/	/	/	0.03	0.0397	0.002	/

steel	C	Cr	Mo	W	Nb	Ta	V	P	Mn	Ni	B	N	Si
T91	0.1	8.32	0.96	<0.01	0.06	--	0.24	0.02	0.43	0.24	<0.0005	0.03	0.32
E97	0.12	8.96	<0.001	1.1	<0.001	0.13	0.19	<0.005	0.43	0.007	<0.001	0.016	0.07

Normalisation:

for alloys : **1050 °C for 3h,**
after air cooling
 for steels: **1040-1070°C for 1h**

Tempering:

for alloys : **730°C for 4 h 10min,**
after air cooling
 for steels: **730-780°C for 1h**

Experimental characterisation techniques (before and after irradiation)

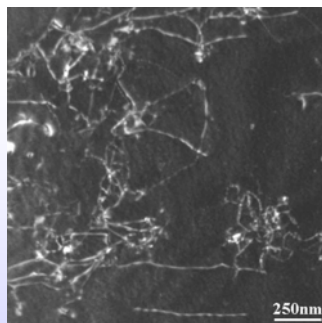
Microstructure:

- Metallography / Optical Microscopy
- SEM (Scanning Electron Microscopy)
- TEM (Transmission Electron Microscopy) JOEL 3010:
 - 1 mm disk specimen technique (magnetism)
 - Bright field (BF), Dark field (DF)
 - Weak beam dark field (WBDF), g(4g-6g)
- PAS

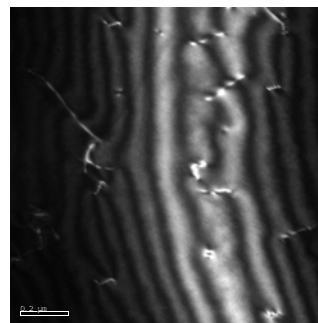
Mechanical properties:

- Hardness (HV5)
- Tensile testing
- Charpy
- Small punch
- Fracture toughness
- Compression (EPFL/CH)

Microstructure of pure Fe and ultra high pure Fe-9Cr before irradiation



Pure Fe

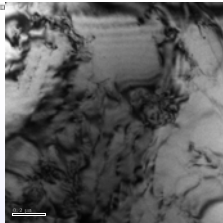


Pure Fe-9 Cr

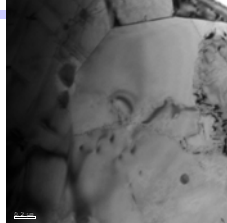
- Ferrite , with grains size from 15-25 μm
- Dislocations are of type $b = a/2 \langle 111 \rangle$, and their density is ($1.7 \times 10^9 \text{ cm}^{-2}$ for FeCr, and $7 \times 10^8 \text{ cm}^{-2}$ for Fe)



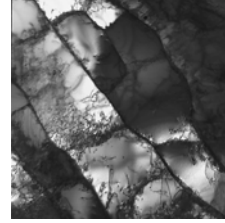
TEM micrographs with microstructure of Fe-Cr alloys and steels before irradiation



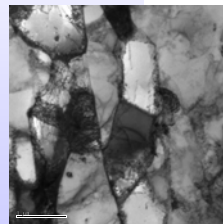
Fe-2.56 %Cr



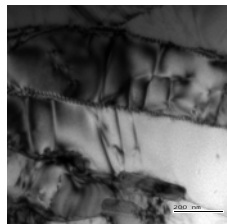
Fe-4.62 %Cr



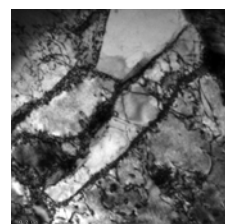
Fe-8.39 %Cr



Fe-11.62%Cr



T91



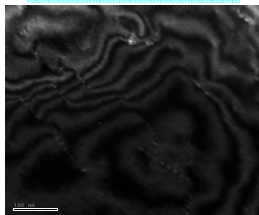
Eurofer 97

the structure changes from fully ferritic to ferrite + bainite: grain size decreases



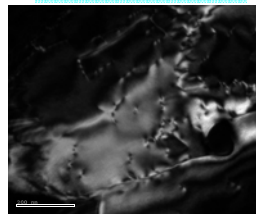
Dislocation structures in unirradiated material with their density

$\rho = 1.2 \times 10^9 \text{ cm}^{-2}$



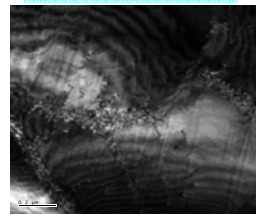
Fe-2.56%Cr

$\rho = 5.8 \times 10^9 \text{ cm}^{-2}$



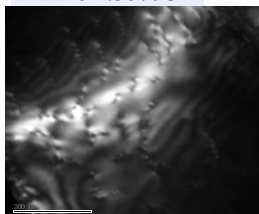
Fe-4.62%Cr

$\rho = 6.3 \times 10^9 \text{ cm}^{-2}$



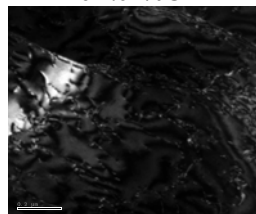
Fe-8.39%Cr

$\rho = 5.5 \times 10^9 \text{ cm}^{-2}$



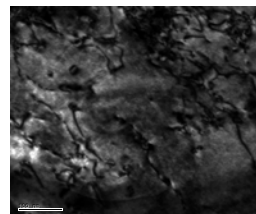
Fe-11.62%Cr

$\rho = 4.7 \times 10^9 \text{ cm}^{-2}$



T91

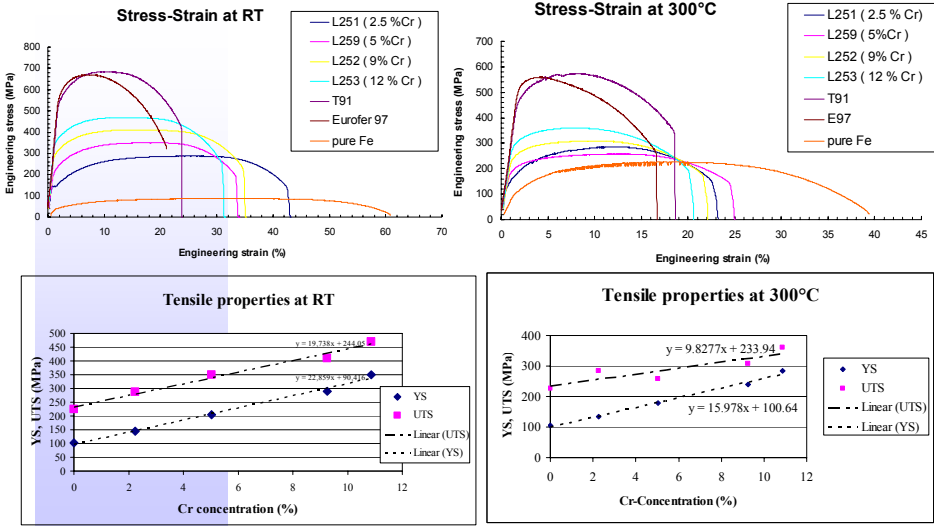
$\rho = 7.8 \times 10^9 \text{ cm}^{-2}$



Eurofer 97



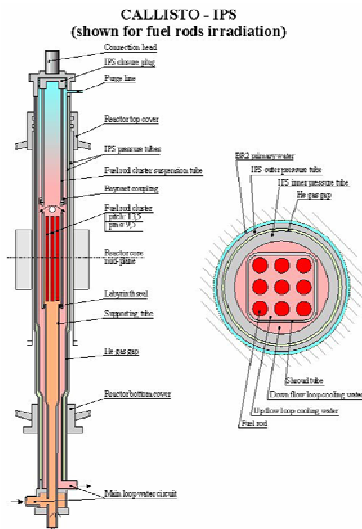
Tensile tests



Irradiation in BR2 (MIRE-Cr)

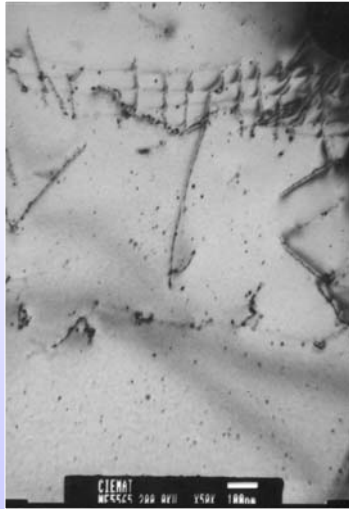
Irradiation conditions:

- Temperature: 300°C
- Pressure: 1.0 MPa ≤ P ≤ 15.7 MPa
- neutron flux (> 1MeV) : 10¹³ n/(cm²s)
- 3 groups of specimens for 1, 3 & 5 cycles
- 3 doses of 0.06, 0.6 and 1 dpa

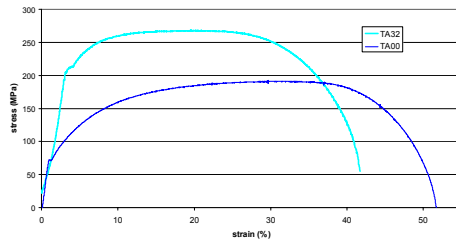
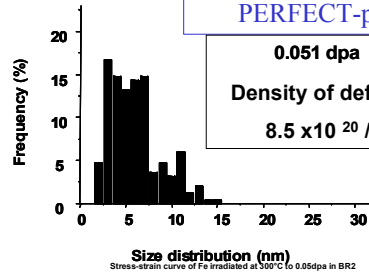




Microstructure of pure Fe after irradiation at BR2

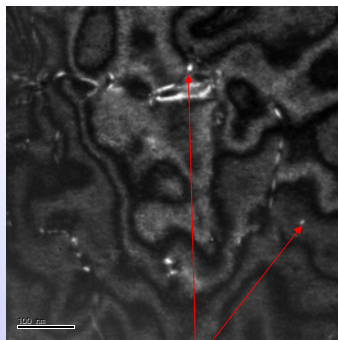


Pure Fe

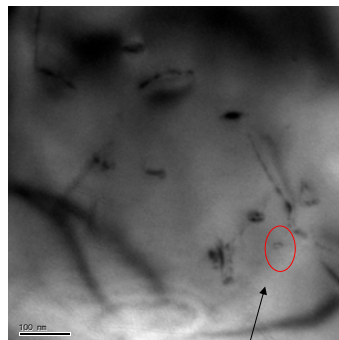


Defects induced by irradiation

- Need of WBDF (g, 4-6g) imaging technique:
[Example for 2.5 % Cr alloy with <110> image condition:](#)

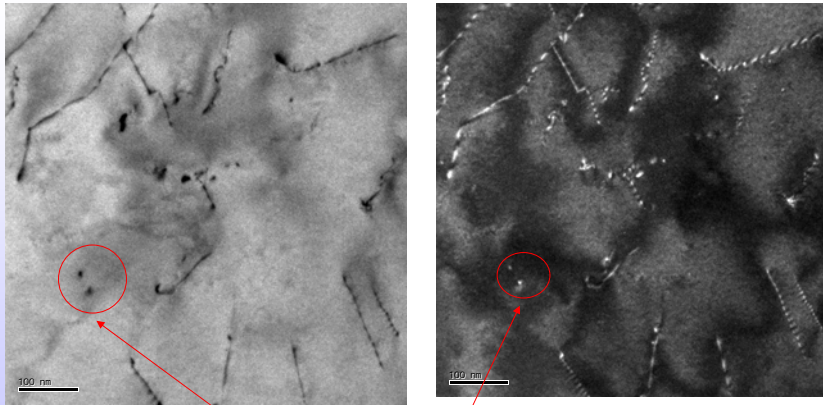


Defects
 $d = 6-8 \text{ nm}$, $\rho = 0.7 \times 10^{21} / m^3$



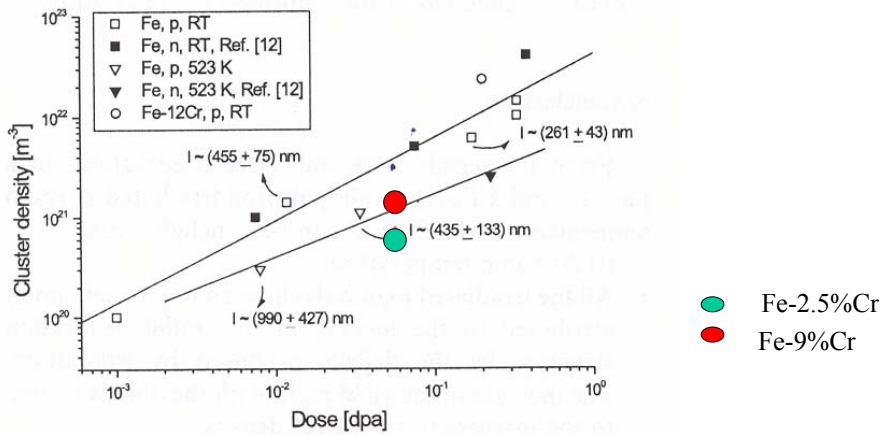
small loop
 $d = 12 \text{ nm}$

Fe-9% Cr alloy after irradiation



Defects , $d = 4 - 7 \text{ nm}$ and $p = 1.325 \times 10^{-21} / \text{m}^3$

Dose dependence of the defect density in Fe and Fe-Cr alloys

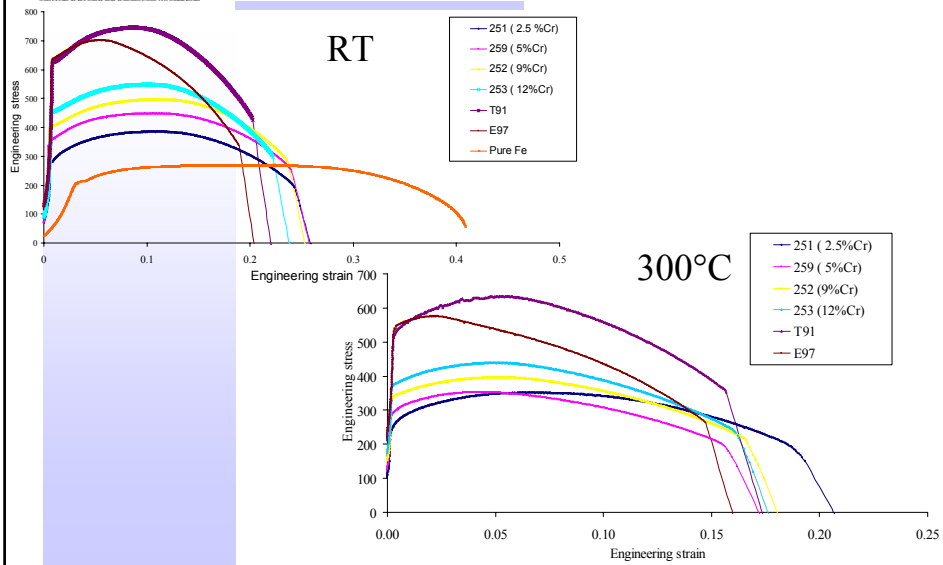


M.I.Luppo et al. JNM(2000)



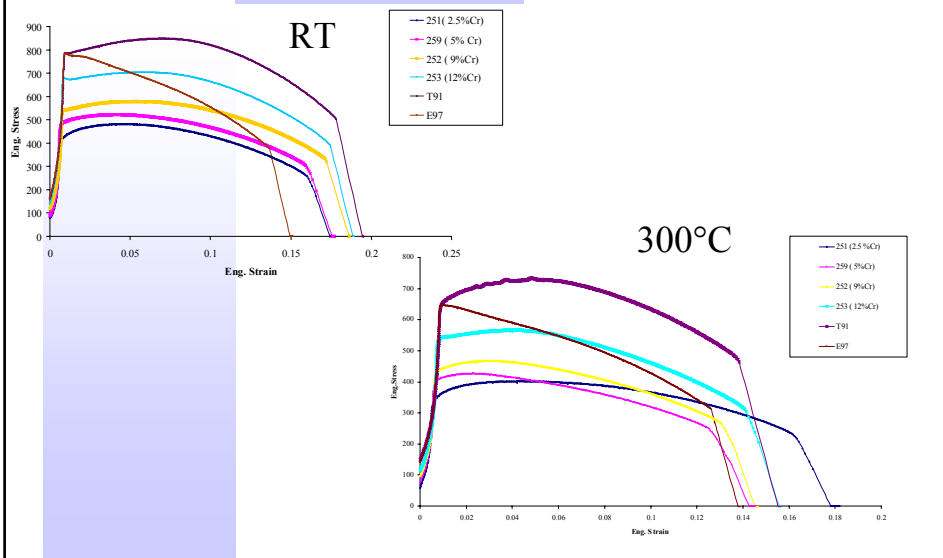
Tensile test at RT and 300°C for 0.06 dpa

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Tensile test at RT and 300°C for 0.6 dpa

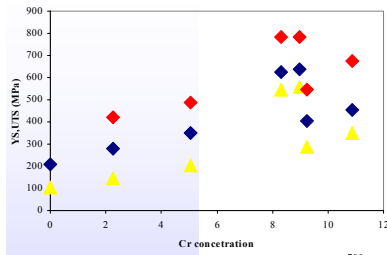
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CENTRE D'ETUDE DE L'ENERGIE NUCLEAIRE





Tensile properties and their comparison

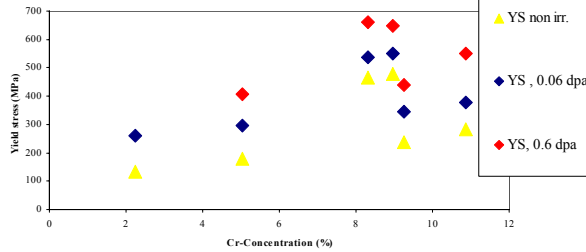
RT



Neutron irradiation at 300°C results in hardening of Fe-Cr alloys and it increases with doses

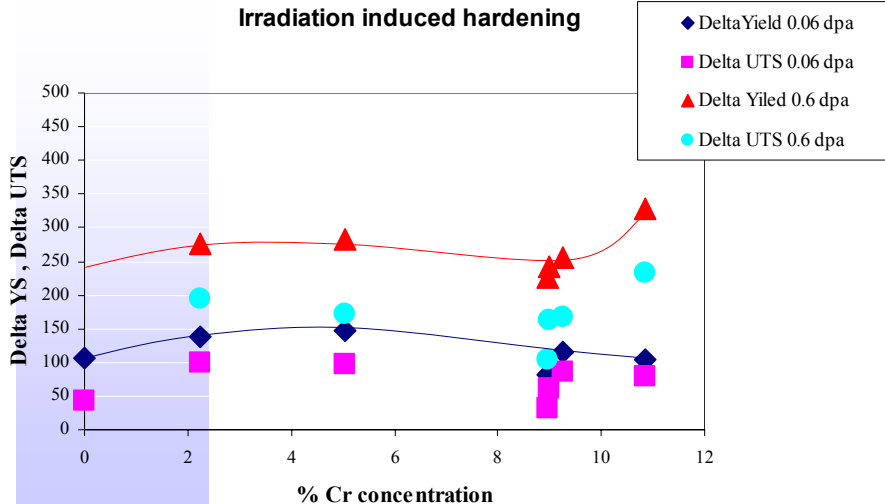
Increase of YS can be observed, as well as loss of ductility, compared with non-irradiated material

300 °C

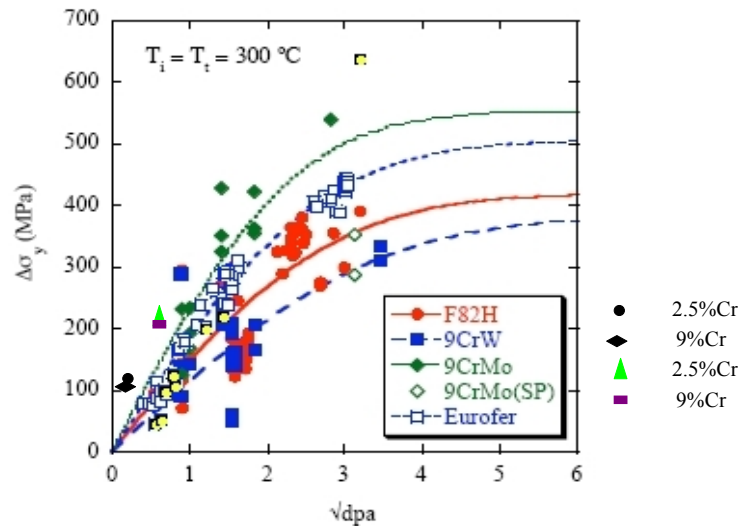


Hardening

Irradiation induced hardening



Comparison with other FM steels



Summary after irradiation at 300°C for doses of 0.06 dpa and 0.6 dpa

- Microstructure showed small defects induced by irradiation (**work is still in progress**)
- Neutron irradiation results in hardening of Fe-Cr alloys followed by reduction of their ductility
- The hardening depends on Cr concentration and it increases with doses of irradiation

Outlook

- The irradiation campaign should finish by end 2005
- 2005-2006 will hence be needed for PIE, using all mentioned techniques
- The combination of characterisation techniques on model materials will provide data on both microstructure and mechanical properties for systems close to steels
- These data will both be useful for model validation and to allow a wide correlation (model alloys, steels, ...) between microstructure, composition and mechanical behaviour under irradiation