



Water vapour corrosion of rare earth disilicates (RE₂Si₂O₇) in flowing hot atmospheres containing Al(OH)₃

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- Sample evolution during corrosion
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- Summary





Introduction

Why corrode rare earth disilicates?

 $RE_2Si_2O_7$: candidates for EBC materials for the protection of Si-based ceramics (SiC, Si₃N₄) in hot wet environments

SiC + $3H_2O(g) \rightarrow SiO_2 + 3H_2(g) + CO(g)$ Si₃N₄ + $6H_2O(g) \rightarrow 3SiO_2 + 2N_2(g) + 6H_2(g)$

$SiO_2 + 2H_2O \rightarrow Si(OH)_4(g)$



From: Nickel et al (2000) in Riedel: Handbook of Ceramic Hard Materials, VCH Weinheim





Introduction

Rare earth disilicates

 $RE_2Si_2O_7 + 2H_2O \rightarrow RE_2SiO_5 + Si(OH)_4(g)$

Low silica activities \rightarrow less volatility / material loss than SiC, Si₃N₄

Low CTE mismatch $RE_2Si_2O_7 \Leftrightarrow SiC / Si_3N_4$



From: Klemm et al (in press) Proc. Cocoa Beach meeting 2004





Introduction

Expected corrosion behaviour

 $RE_2Si_2O_7 + 2H_2O \rightarrow RE_2SiO_5 + Si(OH)_4(g)$



From: Yuri et al (2004) Proc. ASME Turbo Expo 2004





Introduction

Intentions

- * Up to now: only scarce and sometimes contadictory corrosion data for RE₂Si₂O₇
 - \rightarrow new data for a better understanding
- * Better corrosion resistance of $RE_2Si_2O_7$ with small rare earth ions?

→ New findings concerning the hydro corrosion of $RE_2Si_2O_7$ in the presence of AI impurities





Sample preparation and experimental setup

Pressureless sintering of oxide powder mixtures

 \rightarrow Disilicates of

Lu	Yb	Υ
50%¥ 50%Lu		50%¥ 50%Yb
75%¥ 25%Lu		75%¥ 25%Yb





Sample preparation and experimental setup

50 µm

Sintering densities







Sample preparation and experimental setup



$$T = 1500^{\circ}C$$
, $v_{gas} = 13$ cm/s, $p_{total} = 1$ bar, $p_{H2O} = 0.3$ bar





Sample evolution during corrosion

Weight losses



→ No simple linear kinetics as expected → Corrosion behaviour ≠ expectations





Sample evolution during corrosion



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Sample evolution during corrosion

Evolution of the upper faces



10 µm

(50Y 50Yb)₂Si₂O₇, 120 h corrosion time



 $(50Y 50Yb)_2Si_2O_7$, 310 h corrosion time



(75Y 25Lu)₂Si₂O₇, 310 h corrosion time

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Sample evolution during corrosion

Evolution of the upper faces



Garnet RE₃Al₅O₁₂

<u>Highly porous Y₂Si₂O₇:</u>

Strong corrosive alteration reaches deep into the bulk

Apatite $RE_{9.33}(SiO_4)_6O_2$ with Ca





Sample evolution during corrosion

Evolution of the lower faces

First sample in the sequence: Lu₂Si₂O₇







Sample evolution during corrosion

Evolution of the lower faces



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Theory for the observed phase development



From: Fabrichnaya et al (2001): Z.Metallkd. 92



Calculated by O. Fabrichnaya on the basis of data from Fabrichnaya et al (2001): Z. Metallkd. 92





Theory for the observed phase development

Evolution of the upper faces





* Si loss from the melt





Theory for the observed phase development

Evolution of the upper faces





* Further Silica loss: formation of Garnet

* In later stages: formation of Monosilicate / Apatite possible





Theory for the observed phase development

Evolution of the upper faces





 * Formation of a subsurface layer (with low contents of AI and Si) by diffusion of elements





Theory for the observed phase development

Evolution of the lower faces









Theory for the observed phase development

Evolution of the lower faces









General behaviour of the weight loss curves in accordance with corrosion model:

* High losses in an initial stage when a silica-rich melt interacts with the gas phase * Slower (linear) rates in later stages when a melt with a fixed, lower silica activity interacts with the atmosphere







Mass losses



corrosion time (h)







Mass losses



Weight loss rates (*10⁻³ mg/cm²h)

_	50%Y	50%Y	75%Y	75%Y		
Yb	50%Lu	50%Yb	25%Lu	25%Yb	Y	SiO ₂
1.34	0.76	0.95	0.64	0.73	0.96	7.21
Ų	₩	Ų	Ų	↓	₩	
2.68	1.52	1.90	1.28	1.46	1.92	

Gas flow direction

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Only limited significance of the measured weight loss rates

1) Saturation effects show clear influence on corrosion / weight loss rates



2) Al uptake: corrosive alteration connected with weight gain

→ as long as Al uptake cannot be quantified: measured weight loss gives no information about extent of material damage





Comparison with literature data

Literature data: T, v_{gas}, p_{H2O}, p_{total} Gas diffusion model $\rightarrow \rightarrow \rightarrow \rightarrow \rightarrow \rightarrow \rightarrow$ (E. J. Opila and others) $\overline{T} = 1500^{\circ}\overline{C}$ $V_{gas} = 13 \text{ cm/s}$ $p_{H2O} = 0,3 \text{ bar}$ $P_{total} = 1 \text{ bar}$

$$K_{I} \propto (v_{gas}^{1/2} * p_{H2O}^{2}) / p_{total}^{1/2}$$
$$K_{I} \propto exp (E_{a} / RT)$$

(simplified expressions)







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Higher corrosion rates in atmospheres containing AI(OH)₃

1) Intensifying effect of AI(OH)₃ on the silica loss from the samples?

2) $Si(OH)_4$ saturation of the gas phase when SiC or SiO_2 furnace tubes are used?





<u>Summary</u>

- * Hydro corrosion behaviour of $RE_2Si_2O_7$ with AI contamination different from the behaviour without it
- \rightarrow Corrosion by the formation of a melt which loses Si to the atmosphere
- → Layered structure: garnet at the surface, silica depleted phases without Al below
- \rightarrow Corrosive alteration reaches deep into the material
- \rightarrow Formation of new phases can cause cracking
- → Fast weight loss rates in an early stage of corrosion, slower rates after some hours
- → Weight loss rates > weight loss rates measured without AI contamination in SiC tubes (despite saturation and AI incorporation effects)





Thank you for your attention!

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